PATENT APPLICATION

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TITLE OF THE INVENTION:

PHYSIOLOGICAL TOTAL KNEE IMPLANT

INVENTOR:

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STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH OR DEVELOPMENT Not Applicable

FIELD OF THE INVENTION

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The present invention relates to total knee arthroplasty and, more particularly to an improved meniscal component for both fixed bearing and mobile bearing prostheses.

BACKGROUND OF THE INVENTION

Total knee prostheses can be divided into two general categories: fixed bearing and mobile bearing. Both the fixed and mobile bearing knee prosthesis includes a femoral component, a tibial component, and a meniscal component, or bearing, which is located between the femoral component and the tibial component. In the conventional fixed bearing prosthesis, the bearing is fixedly attached to the tibial component. In the conventional mobile bearing prosthesis, the bearing is allowed some limited range of symmetrical motion. The form of the prosthetic knee joint selected by the orthopedic surgeon depends upon the condition of the natural knee and the age, health and mobility of the patient.

Fixed bearing prostheses are generally indicated where there is severe damage to the femurand/or tibia or when neither the posterior nor anterior cruciate ligaments can be retained. The fixed

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bearing prosthesis generally does not allow correction for a misplacement in rotation on the tibial

component and may contribute to accelerated wear of the bearing component due to high contact

stresses. Congruency between the femoral and tibial articulating surfaces must be balanced to

provide maximum contact area, which lowers the stresses on the bearing without constraining the

normal movement of the femur on the tibia, which could result in high shear stress. During deep

knee flexion, congruency may be lost resulting in direct, repetitive contact between the femoral and

tibial components. Prior art fixed bearing prostheses have not addressed this concern.

Mobile bearing prostheses were developed in an effort to replicate the normal biomechanics

of the natural knee joint and are generally indicated for patients who have adequate collateral

ligament stability. Many prior art mobile bearing prostheses are limited to a simple rotation, which

in some instances is coupled with constrained anterior-posterior translation. In these systems, the

displacement of the lateral portion of the bearing component about the axis of rotation is generally

symmetrical, which causes the femoral component to strike and erode the bearing component due to

the asymmetrical characteristic of femoral rollback. Other prior art mobile bearing prostheses are

limited to anterior-posterior translation in the absence of rotational misalignment correction, thus do

not conform to natural biomechanical movement.

Accordingly, a fixed bearing prosthesis and a mobile bearing prosthesis are disclosed. The

fixed bearing prosthesis comprises generally a tibial component, a femoral component and a

meniscal component disposed between the tibial and femoral components and addressees the loss of

congruency during deep knee flexion and the possible direct, repetitive contact of the tibial and

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femoral components. The tibial component of the fixed bearing prosthesis includes a tibial platform having an anterior and posterior edge. The meniscal component of the fixed bearing prosthesis includes a posterior ridge overlapping the posterior edge of the tibial platform that prevents metal-to-metal contact during deep knee flexion. The mobile bearing prosthesis comprises generally a tibial component, a femoral component and a meniscal component disposed between the tibial and femoral components and addresses the lack of conformity to natural biomechanical movement. The tibial component comprises a tibial platform having a curved rail system designed to mimic the asymmetrical rotation of femoral rollback while simultaneously providing sufficient anterior-posterior translation.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 illustrates a conventional fixed bearing prosthesis.

Figure 2 illustrates condylar liftoff with a conventional fixed bearing prosthesis and the possibility of direct metal-to-metal contact between the femoral and tibial components.

Figure 3a is a rear perspective view of one preferred embodiment of a fixed bearing prosthesis featuring an improved meniscal component.

Figure 3b is a side perspective view of one preferred embodiment of a fixed bearing prosthesis featuring an improved meniscal component.

Figure 4 is a side perspective view of the tibial component of one preferred embodiment of a mobile bearing prosthesis in accordance with the present invention.

Figure 5 is a top perspective view of the tibial component shown in Figure 4.

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Figure 6 is a front perspective view of the meniscal component of one preferred embodiment

of a mobile bearing prosthesis in accordance with the present invention.

PREFERRED EMBODIMENTS OF THE INVENTION

In the following detailed description of the preferred embodiments, reference is made to the

accompanying drawings, which form a part hereof, and in which are shown by way of illustration

specific embodiments in which the invention may be practiced. It is to be understood that other

embodiments may be utilized and structural changes may be made without departing from the scope

of the present invention.

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Movement of the natural knee joint can be classified as having 6 degrees of freedom: three

translations, including anterior/posterior, medial/lateral, and inferior/superior; and three rotations,

including flexion/extension, internal/external, and adduction/adduction. Movements of the knee

joint are determined by the shape of the articulating surfaces of the tibia and femur and the

orientation of the four major ligaments of the knee joint, including the anterior and posterior cruciate

ligaments and the medial and lateral collateral ligaments.

Knee flexion/extension involves a combination of rolling and sliding called femoral rollback.

Because of asymmetry between the lateral and medial femoral condyles, the lateral condyle rolls a

greater distance than the medial condyle during knee flexion. This causes coupled external rotation

of the tibia, which has been described as the "screw-home" mechanism of the knee that locks the

knee into extension. During deep knee flexion, the lateral femoral condyle may roll back sufficiently

to loose contact with tibia, a phenomena known as condylar liftoff.

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As stated above, the orientation of the four major ligaments in the knee play a role in

determining movement of the joint. The primary function of the medial collateral ligament is to

restrain valgus rotation of the knee joint, with its secondary function being control of external

rotation. The lateral collateral ligament restrains varus rotation and resists internal rotation.

The primary function of the anterior cruciate ligament is to resist anterior displacement of the

tibia on the femur when the knee is flexed and control the "screw-home" mechanism of the tibia in

terminal extension of the knee. A secondary function of the anterior cruciate ligament is to resist

varus or valgus rotation of the tibia, especially in the absence of collateral ligaments. The anterior

cruciate ligament also resists internal rotation of the tibia.

The primary function of the posterior cruciate ligament is to allow femoral rollback in flexion

and resist posterior translation of the tibia relative to the femur. The posterior cruciate ligament also

controls external rotation of the tibia with increasing knee flexion.

The natural knee joint can become damaged or diseased such that the articular surfaces of the

femur or tibia may deteriorate and cause damage to the articular cartilage between the bones. In

these instances, total knee arthroplasty is often indicated. However, knee replacement has a finite

expected survival that is adversely affected by activity level. Thus, significant research and

development has been directed to the development of knee prostheses that minimize the possibility

of dislocation, bearing failure and loosening from the bones, and that significantly imitates the

natural motion of the knee joint.

The design of any total knee replacement must provide appropriate joint function and range

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of motion, transfer the large loads that cross the joint from the implant components to the

surrounding bone, and allow for long-term use without severe wear to the implant surfaces. In

addition to selecting the appropriate design, the surgeon must also determine whether to sacrifice or

retain the posterior cruciate ligament.

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Fixed bearing prostheses meet these design requirements by having bicondylar geometries

with curved surfaces in both the anteroposterior and medial-lateral directions. The appropriate

choice of radii of curvatures for the tibial and femoral components minimizes contact stresses, while

providing adequate restraint. In the instances when the posterior cruciate ligament is sacrificed, the

prosthesis typically incorporates a femoral cam and tibial spine to control femoral rollback and

prevent anterior sliding and posterior subluxation of the knee.

On the other hand, mobile bearing prostheses allow for more natural joint kinematics, while

also allowing the articulating surfaces to be more conforming than a fixed-bearing knee, leading to

larger contact areas, lower contact stresses, and better wear resistance.

As shown in Figure 1, conventional fixed bearing prostheses generally comprise a tibial

component 1, a femoral component 2 and a meniscal component 3 disposed between the tibial

component 1 and femoral component 2. The meniscal component 3 is locked into the tibial

component 1 and does not move from the tibial tray 4. The meniscal component 3 provides a surface

5 where the articular surface 6 of the femoral component 2 can slide without any significant friction.

Figure 2 illustrates condylar liftoff during deep knee flexion. The lateral condyle 7 of the

femoral component 2 lifts off of the meniscal component 3 during femoral rollback. With deep knee

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flexion, the metal surface of lateral condyle 7 may come into direct and repetitive contact with the

metal surface of the tibial tray 4 of the tibial component 1.

Figures 3a and 3b show one preferred embodiment of a fixed bearing prosthesis of the

present invention that addresses the potential metal-to-metal contact between the lateral condyle 7 of

the femoral component 2 and the tibial tray 4. As seen in Figure 3a, the tibial component 10 of the

fixed bearing prosthesis comprises a tibial tray 12 and a fixed bearing 13 that is fixedly attached to

the tibial tray 12. The fixed bearing 13 comprises a posterior ridge 15 that overlaps the posterior

edge 16 the tibial tray 12. Figure 3b shows the same fixed bearing prosthesis in a side perspective

view.

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The femoral component and the tibial components of the fixed bearing prosthesis of the

present invention may be made of any conventional biocompatible material, including but not limited

to, titanium, titanium alloy, cobalt-chrome, alumina or zirconia ceramic. The femoral and tibial

components may be fixed by cement, a hydroxyaptite coating, or by any other conventional means.

The shape of the meniscal component, the fixed bearing, has a generally planar inferior

surface with a generally downward extending posterior ridge that overlaps the posterior edge of the

tibial tray. The superior surface of the meniscal component may include one or more generally

concave depressions to match the generally convex surfaces of the condylar portions of the femoral

component. The meniscal component may be made of any conventional biocompatible material,

however, ultra high molecular weight polyethylene is typically employed.

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Mobile bearing knee prostheses reduce meniscal component wear and mimic the normal

biomechanics of the natural knee joint. The mobile bearing prosthesis of the present invention is not

limited to a simple rotation. The meniscal component is allowed to slide along curved rail that

forces the knee to follow a more normal physiological pattern as opposed to conventional designs.

The radius of the curved rail allows the femoral condyle to rotate and slide on the tibial plateau

imitating the physiological movement of the knee.

Figure 4 illustrates the tibial component 20 of one preferred embodiment of a mobile bearing

prosthesis of the present invention. The tibial component 20 generally comprises a tibial platform 25

having a curved rail 30 designed to mimic the asymmetrical rotation of femoral rollback while

simultaneously providing sufficient anterior-posterior translation. The shape of curved rail 30 may

conform to any conventional rail design, such as a dovetail or T-shaped rail. However, the preferred

shape of curved rail 30 is a T-shape rail. Figure 5 is a top perspective view of tibial component 20

illustrating the curvature of T-shape rail 30. The tibial platform 25 may be integrally constructed as a

monolithic tibial component, or the tibial platform may be fixedly attached to the tibial component

20 by conventional means.

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The mobile meniscal component 40 is shown in Figure 6. The mobile meniscal component

40 comprises a generally planar inferior surface 42 and a superior surface 44. The inferior surface 42

comprises a keyway 45 that slidingly accepts the T-shaped curved rail 30 of the tibial platform 25.

The keyway 45 extends from the anterior edge 46 of meniscal component 40 to the posterior edge 48.

The curvature of the keyway 45 is substantially similar to the curvature of the T-shaped rail 30 such

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that during deep knee flexion, the meniscal component 40 slides along the T-shaped rail 30 allowing

for asymmetrical rotation as well as anterior-posterior translation. As with the fixed bearing design,

the superior surface of the meniscal component may include one or more generally concave

depressions to match the generally convex surfaces of the condylar portions of the femoral

component and may be made of any conventional biocompatible material, however, ultra high

molecular weight polyethylene is typically employed. The meniscal component 40, as seen in Figure

6, may employ a branched keyway, which would allow the same meniscal component 40 to be used

for either right or left knee arthroplasty.

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Although the present invention has been described in terms of specific embodiments, it is

anticipated that alterations and modifications thereof will no doubt become apparent to those skilled

in the art. It is therefore intended that the following claims be interpreted as covering all alterations

and modifications that fall within the true spirit and scope of the invention.

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